



UNIVERSITY OF PADOVA (ITALY)

DEPT. OF CIVIL, ENVIRONMENTAL AND ARCHITECTURAL ENGINEERING, DICEA



DALLA GASSA SRL

Geotechnical Engineering, Cornedo Vicentino (Vicenza, Italy)

ZABEZPIECZENIE OSUWISK PRZY POMOCY KOTEW SIRIVE®

LANDSLIDE PROTECTION USING SIRIVE® ANCHORS

MSc Ryszard Murzyn (Geo-Inz-Bud, Poland)

Dr Eng Alberto Bisson (Dept. ICEA, University of Padova, Italy)

DALLA GASSA SRL

COMPANY PROFILE

Main activities:

- Excavation support systems: Soil Nailing, Micropiles



- Landslide stabilization, rockfall protection



- Foundations engineering

DALLA GASSA SRL

SIRIVE® PRODUCTION

□ PRODUCTION

Dalla Gassa is the first Italian producer of self-drilling bars (since 2001)



□ CERTIFICATIONS

RINA Certificate
in accordance with
UNI EN ISO 9001:2008

Internal certificate
of the complete
Bar-Nut-Coupling system



DALLA GASSA SRL

SIRIVE® QUALIFICATION

- Qualification as **Official Producer** of Sirive® Self Drilling Bars in accordance with the Italian Ministerial Decree 14/01/2008
- **Certificate of qualification** nr. 002/14-AM for the production of “Self-drilling hollow bars S460J0 with continuous threading, nominal diameter 28 to 38 mm, for passive anchors for geotechnical use”
- **Date: September 9, 2014**
- **Internal laboratory**

autoperforanti
SIRIVE®

ATTESTATO DI QUALIFICAZIONE
002/14-AM

In conformità al D.M. 14.01.2008 “Norme tecniche per le costruzioni”, si attesta che il prodotto da costruzione:

ACCIAIO PER STRUTTURE METALLICHE

Barre cave autoperforanti S460J0 a filettatura continua di diametro nominale da 28 a 38 mm per tiranti di ancoraggio ad uso geotecnico di tipo passivo.

Etichetta di identificazione

etichetta Sirive Autoperforanti R	
LOTTO n°	14072008
COSSA n°	
ACCIAIO n°	
DIAMETRO n°	
DATA PROD.	

prodotto da:
DALLA GASSA s.r.l.
Via Fogazzaro, 71
36073 - CORNEDO VICENTINO (VI)

nello stabilimento di:
via Fogazzaro, 71 – 36073 CORNEDO VICENTINO (VI)

è stato sottoposto da parte del Produttore alle prove di qualificazione del prodotto effettuate a cura del Laboratorio Ufficiale Politecnico di Torino - Dipartimento di Ingegneria Strutturale e Geotecnica e il Servizio Tecnico Centrale del Consiglio Superiore dei Lavori Pubblici ha effettuato l'ispezione iniziale dello stabilimento e del controllo di produzione in fabbrica.

Il presente certificato attesta che tutte le disposizioni riguardanti la procedura di qualificazione definita nella norma

D.M. 14.01.2008: “Norme tecniche per le costruzioni”
sono state applicate.

Il presente attestato ha validità 5 anni dal 18.07.2014 o sino a che le condizioni di produzione in fabbrica o il controllo di produzione in fabbrica non subiscano modifiche significative.

Roma, 9/09/2014

IL DIRIGENTE DELLA DIV. III DEL
SERVIZIO TECNICO CENTRALE
Dott. Ing. Marco Pancalò

PANCALÒ MARCO
COORDINATORE 002/14-AM

ORGANISMO DI QUALIFICAZIONE NAZIONALE ATTESTATO D.M. 14/01/2008

VIA N. BISSOLATI 2 - 00163 ROMA
TEL. 06.4412.4181 - FAX 06.4426.7183

www.cq3.it

DALLA GASSA SRL

RESEARCH & DEVELOPMENT DIVISION

- Advanced **landslide monitoring**
- **Sirive®-1 technical validation**: a «green» Soil Nailing
- PhD on **Sirive® Floating Anchor** for landslide stabilization
- Research & Development of **Sirive® Special Composite Anchor**
- Partnership with **University of Padua** (Italy), **Polytechnic University of Turin** (Italy) and **University of Agriculture in Krakow** (Poland)



Production Control Tutor
for Sirive® Self-Drilling Bars



UNIVERSITY OF AGRICULTURE
IN KRAKOW

DALLA GASSA SRL

AWARDS AND PRIZES



- **Bisson A., Dalla Gassa G. (2013)**
SIRIVE® FLOATING ANCHOR: PATENT AND RESEARCH PROJECT

Galileo Innovators' Festival 2013 - European exhibition on innovation and technology transfer

Special mention at the Micro-Innovation Marathon (2013)



- **Bisson A., Cola S. (2014)**
FLOATING ANCHORS FOR THE STABILIZATION OF SLOW-MOVING LANDSLIDES

CNG 2014: The geotechnical engineering in the defense of land and infrastructure from natural disasters, XXV National Geotechnical Congress, Baveno (Italy), Vol. 2, pp. 327-334
ISBN: 9788897517054

Italian Geotechnical Association Award: best paper for technical-scientific content (2014)



DALLA GASSA SRL

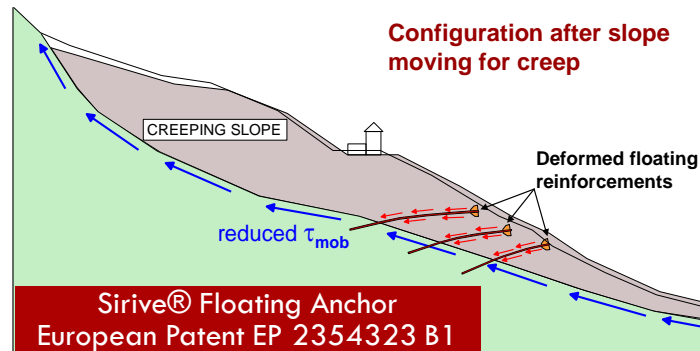
EUROPEAN PATENTS

□ SIRIVE® FLOATING ANCHOR

European Patent

EP 2354323 B1

Date of publication and mention of the grant of the patent: April 1, 2015



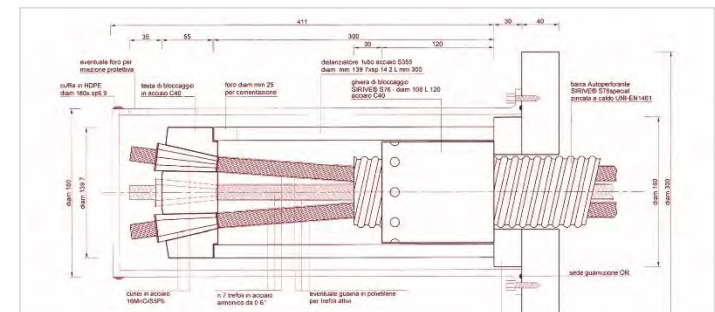
□ SIRIVE® COMPOSITE ANCHOR

European Patent application

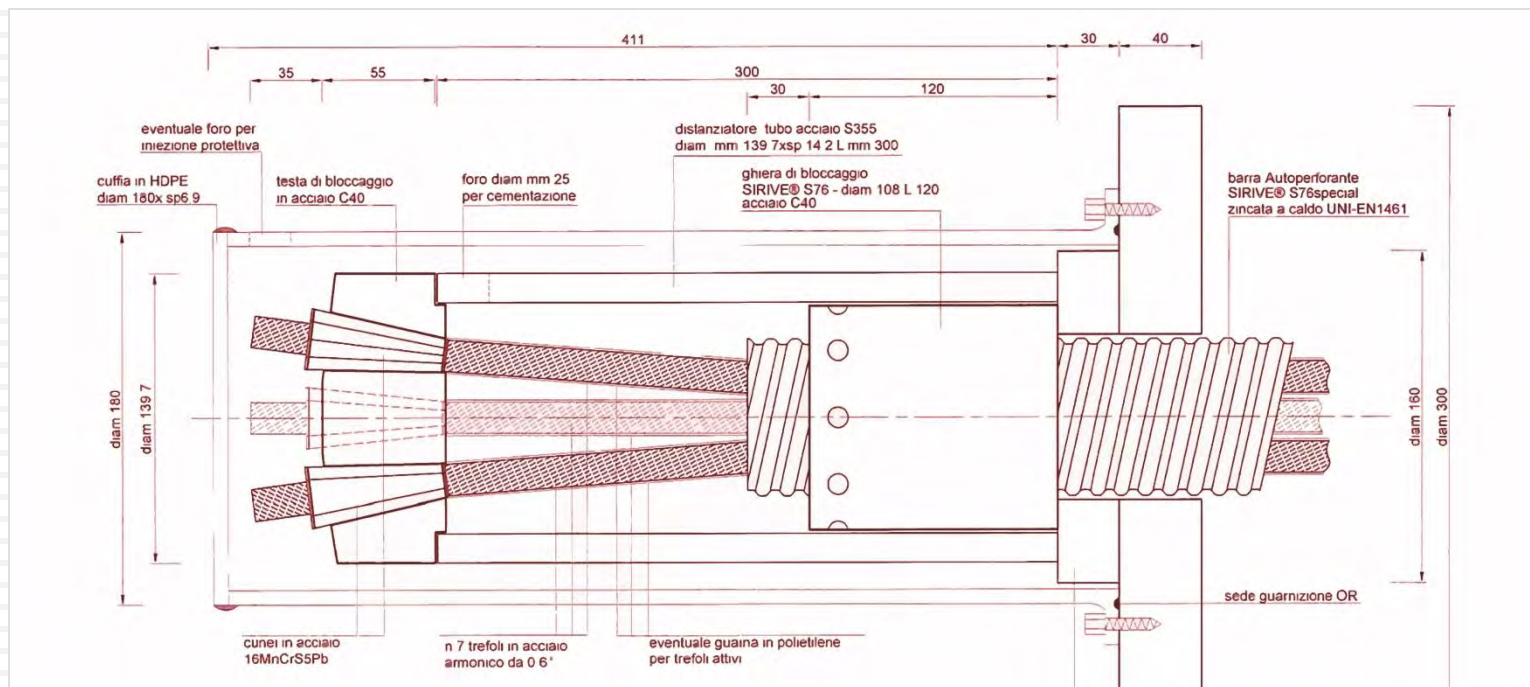
EP 20130157515.1

Date of application: March 1, 2013

The opposition process is still ongoing (2015)

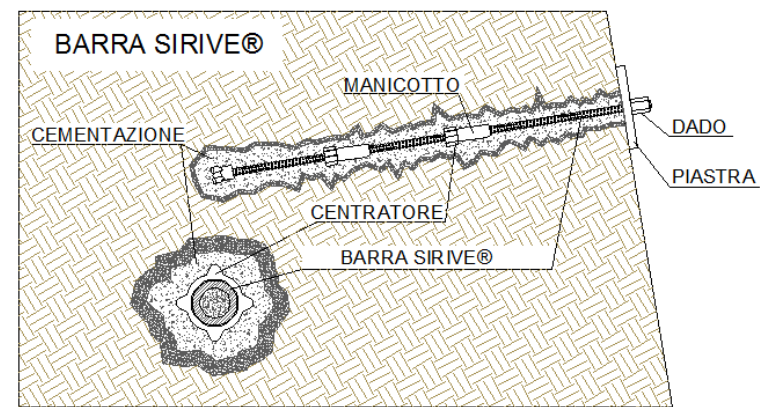


SIRIVE® SPECIAL COMPOSITE ANCHOR



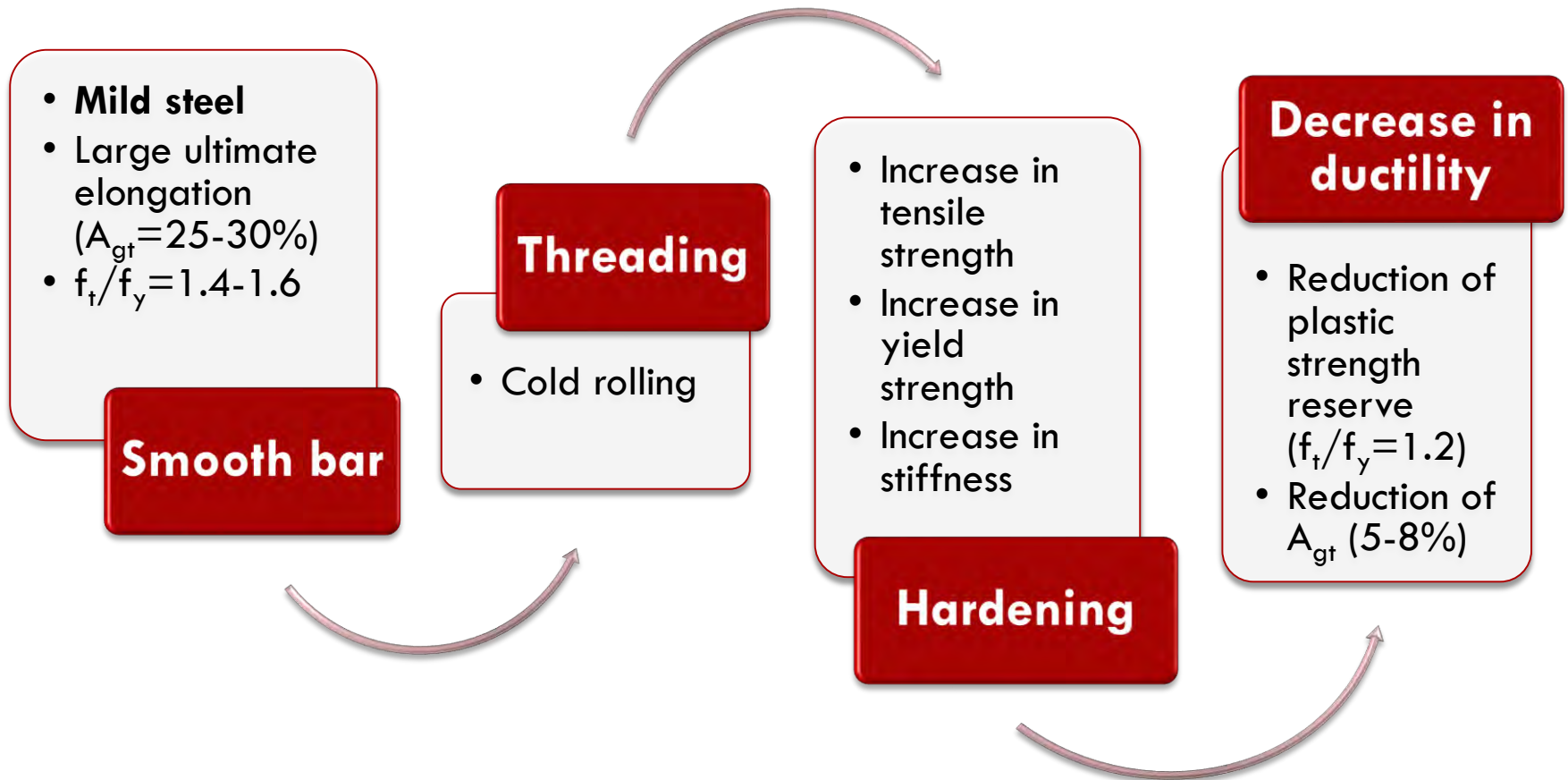
SIRIVE® SELF-DRILLING BARS

- Self-drilling hollow bars cemented along the entire profile (nails)
- **Passive** reinforcements (not pretensioned)
- **Advantages:**
 - ▣ Simple and **fast execution**
 - ▣ Increasing of the diameter of the cemented bulb
 - ▣ Low cost



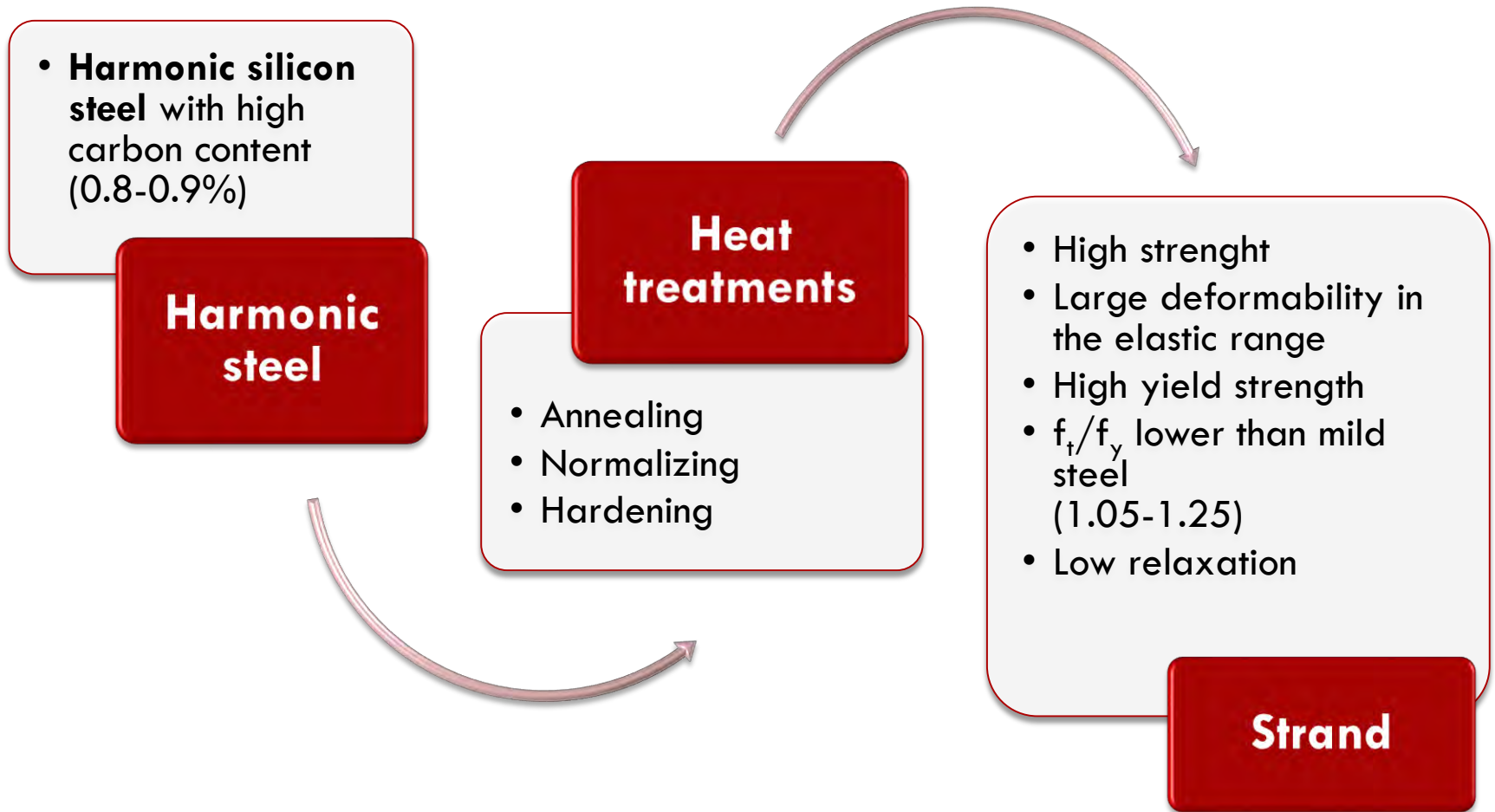
SELF-DRILLING BARS

PRODUCTION PROCESS



STRANDS

PRODUCTION PROCESS



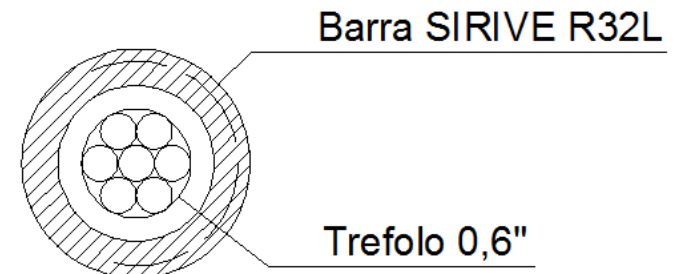
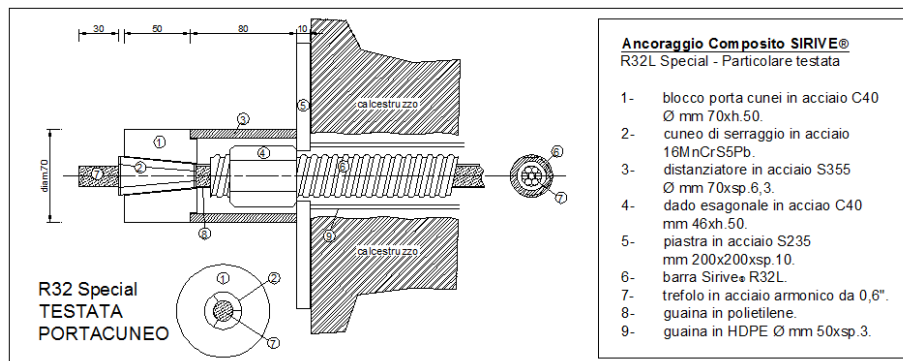
SIRIVE® SPECIAL COMPOSITE ANCHOR

BASIC IDEA

- Goals:
 - ▣ **Serviceability limit state:** increase of the admissible load at constant elongation in the elastic domain;
 - ▣ **Ultimate limit state:** decrease of the plastic deformations at constant elongation.

- Basic idea:

SELF-DRILLING BAR + STRANDS = SIRIVE® COMPOSITE ANCHOR



SIRIVE® SPECIAL COMPOSITE ANCHOR

ANALYTICAL MODEL

□ Main hypotheses:

▣ Congruence of the coupled system

$$\frac{F_b(\sigma)}{E_b(\sigma) \cdot A_b} = \frac{F_t(\sigma)}{E_t(\sigma) \cdot A_t} = \frac{F(\sigma)}{(EA)_{eq}(\sigma)} \quad \text{dove: } A = A_b + A_t$$

▣ Equilibrium of the coupled system

$$F_b(\sigma) + F_t(\sigma) = F(\sigma) = (EA)_{eq}(\sigma) \cdot \frac{\Delta l(\sigma)}{l_0}$$

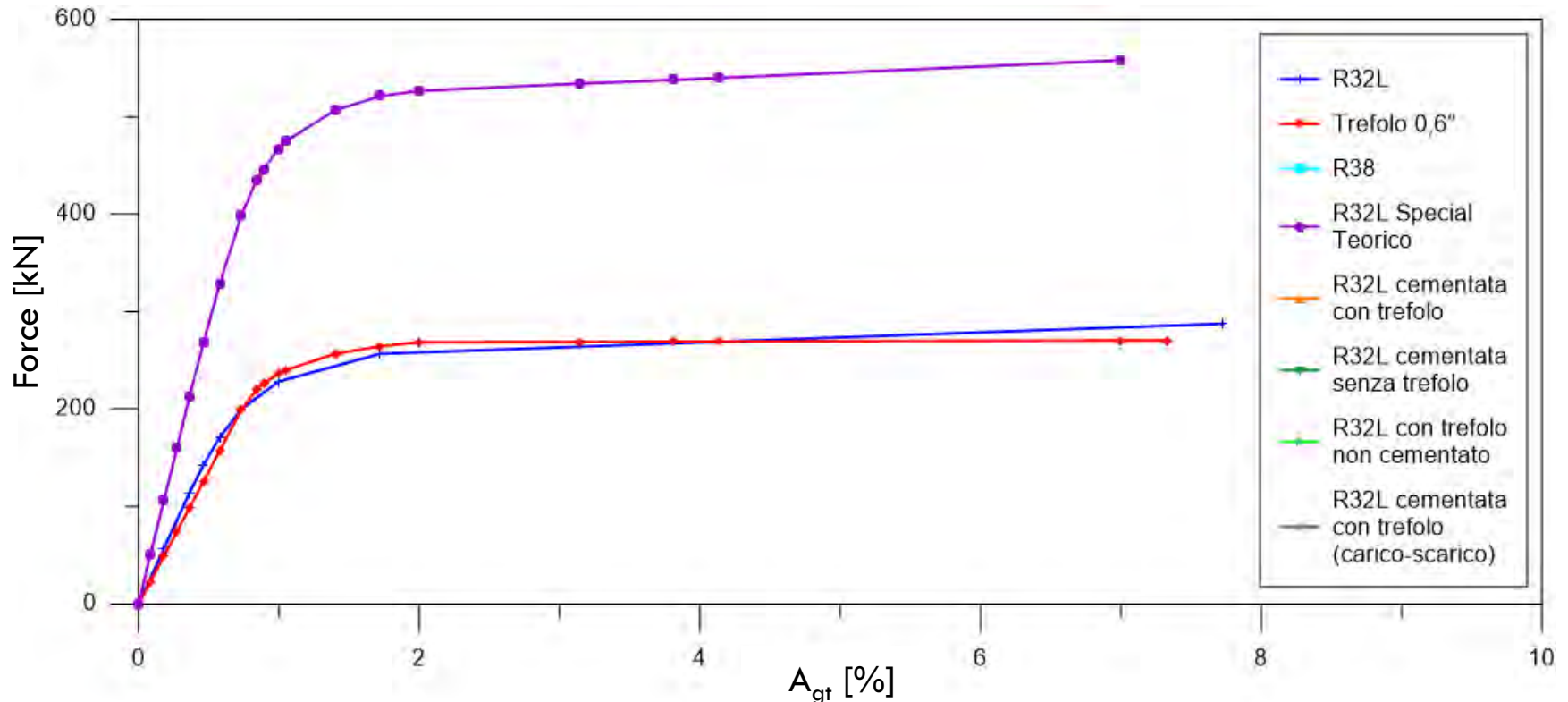
▣ Negligible thermal variations

□ Axial stiffness and elastic modulus **equivalence**:

$$(EA)_{eq}(\sigma) = [E_b(\sigma) \cdot A_b + E_t(\sigma) \cdot A_t] \quad E_{eq}(\sigma) = \frac{[E_b(\sigma) \cdot A_b + E_t(\sigma) \cdot A_t]}{A_b + A_t}$$

SIRIVE® SPECIAL COMPOSITE ANCHOR

EXPERIMENTAL TESTS

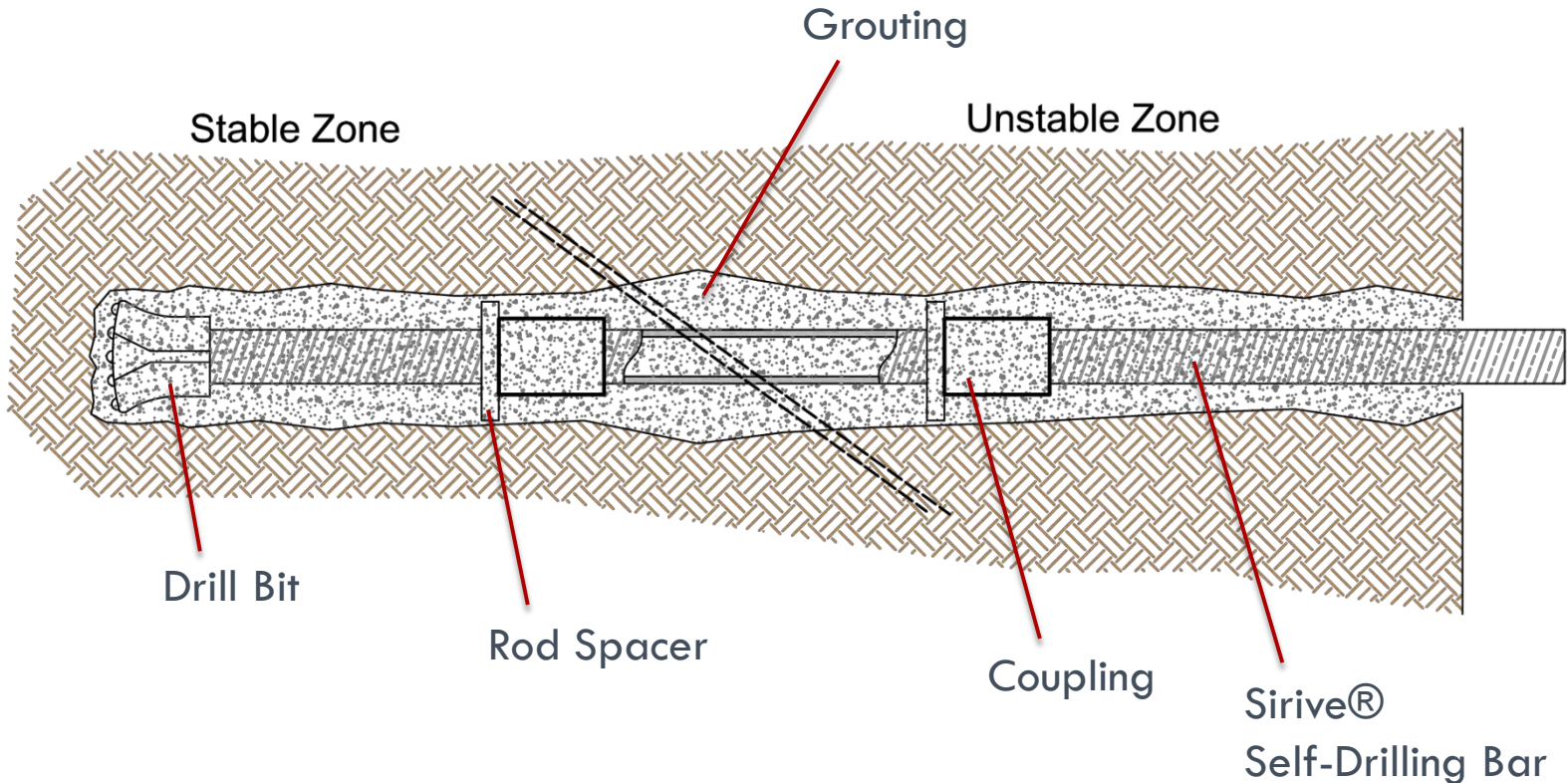


Mechanical behaviour of **R32L Sirive® Self-drilling traditional bar (blue)**, a **0,6'' strand (red)** and **Sirive® Special R32S Composite Anchor (violet)**.

SIRIVE® SPECIAL COMPOSITE ANCHOR

INSTALLATION STEPS FOR ROCK SLOPE STABILIZATION

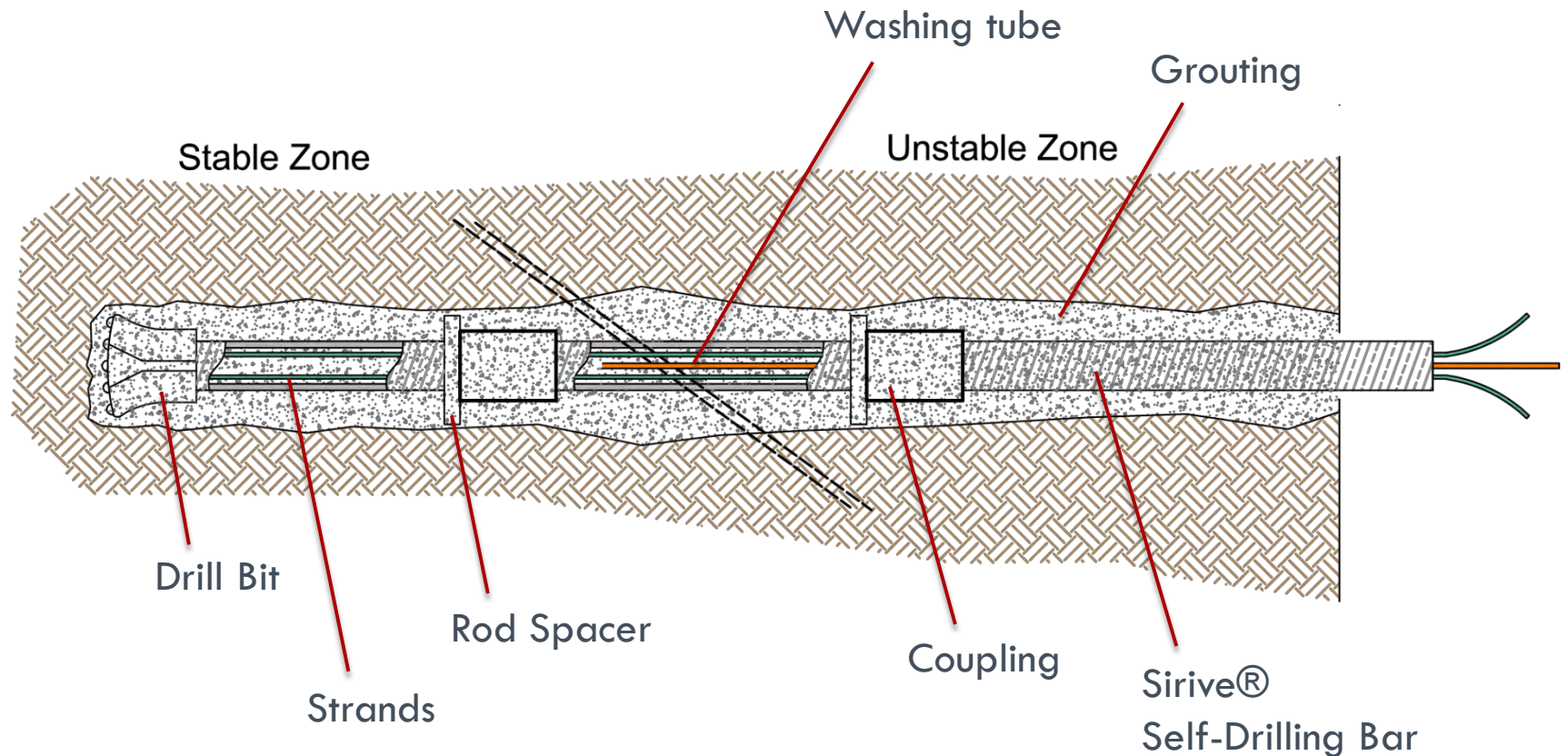
□ **STEP 1:** Installation of the self-drilling bar



SIRIVE® SPECIAL COMPOSITE ANCHOR

INSTALLATION STEPS FOR ROCK SLOPE STABILIZATION

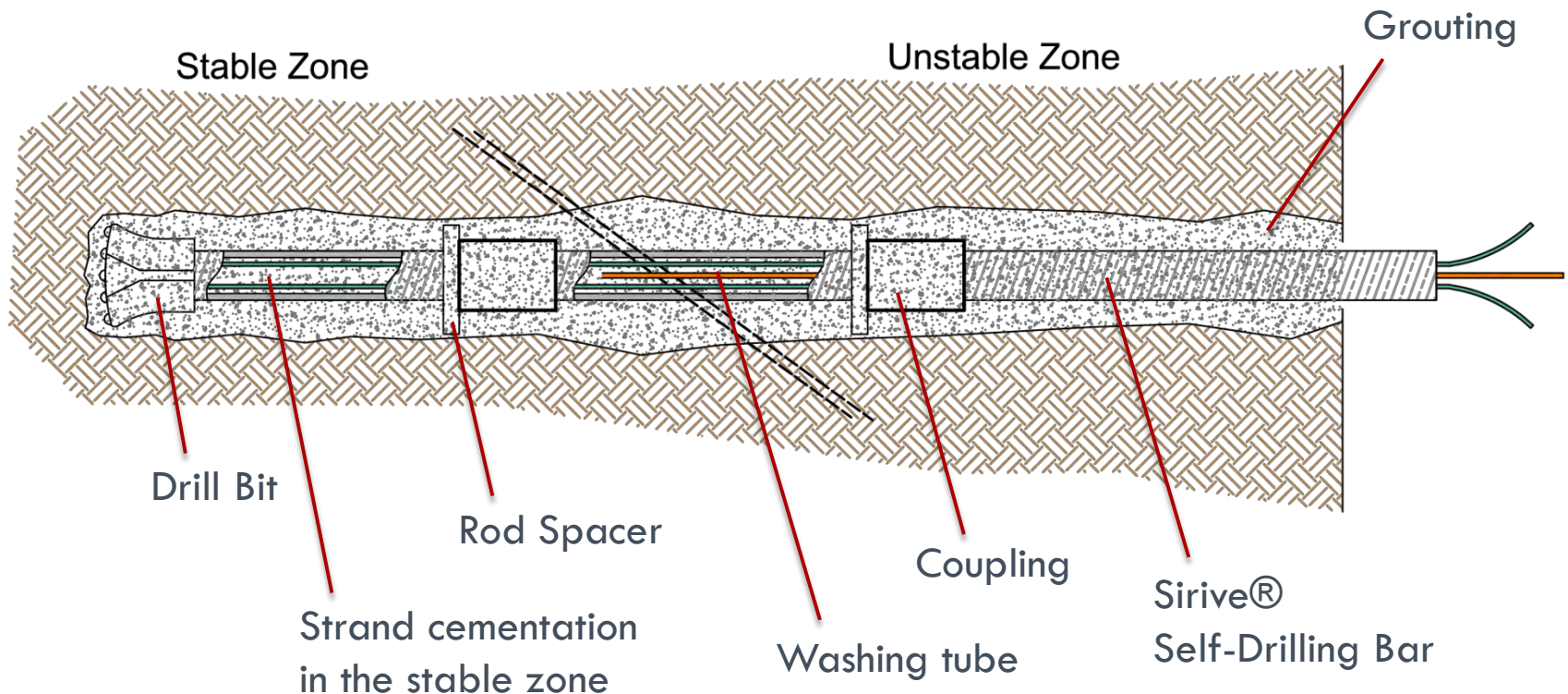
□ **STEP 2:** Installation of strands and washing tube



SIRIVE® SPECIAL COMPOSITE ANCHOR

INSTALLATION STEPS FOR ROCK SLOPE STABILIZATION

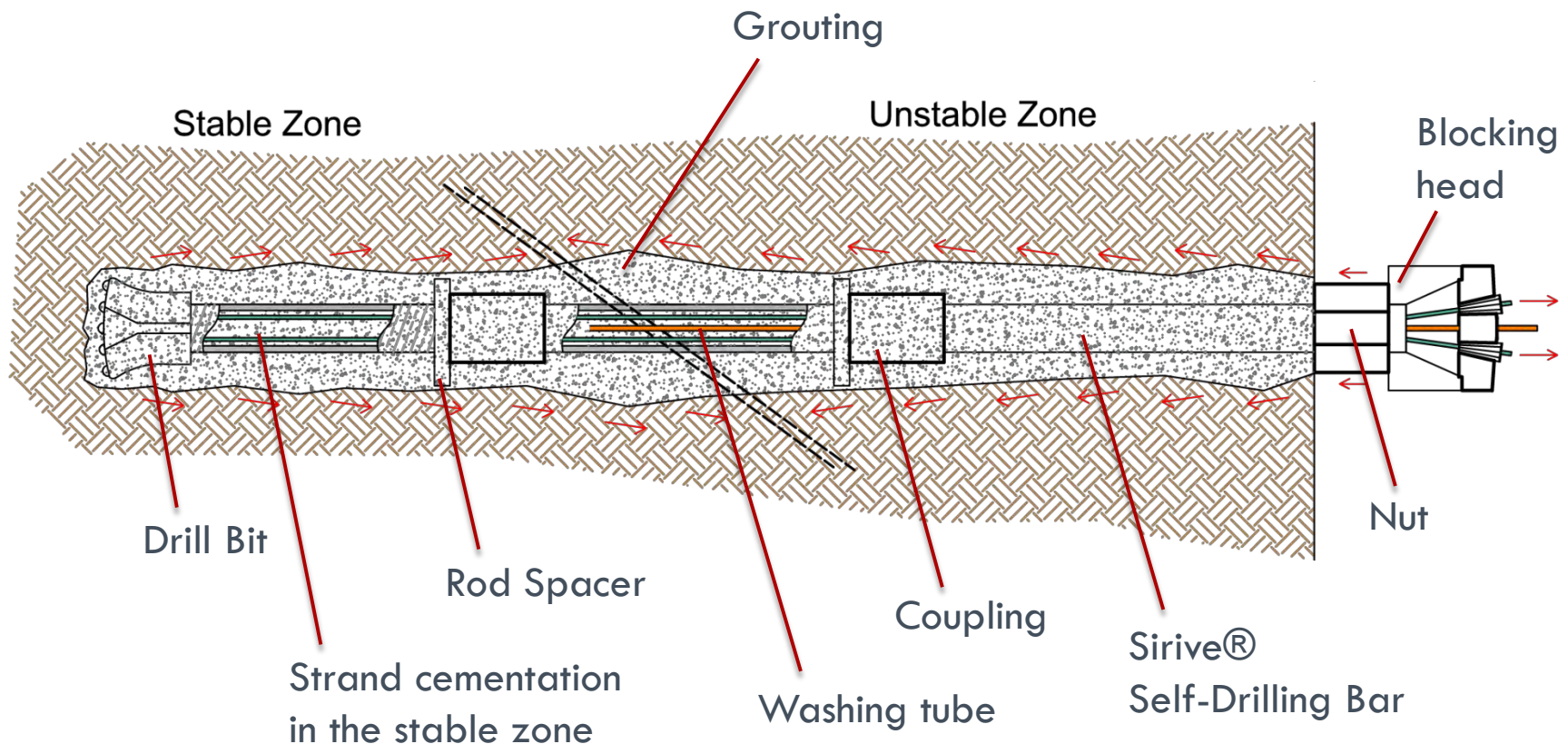
- **STEP 3:** The anchor active zone is washed (with water) and the inner cementation removed (only in the active/unstable part of the anchor)



SIRIVE® SPECIAL COMPOSITE ANCHOR

INSTALLATION STEPS FOR ROCK SLOPE STABILIZATION

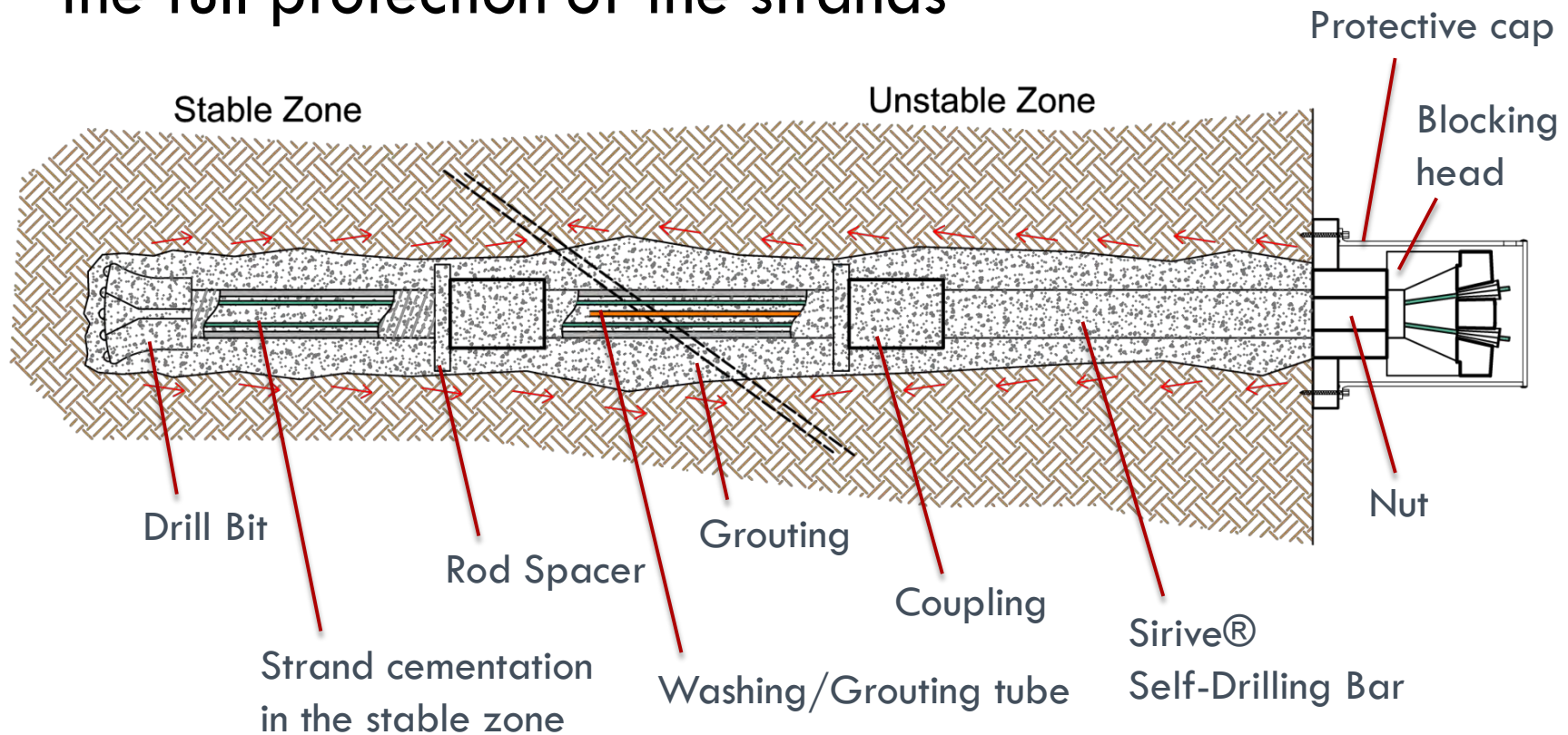
- **STEP 4:** After the grout full maturity, the strands are tensioned at the design load



SIRIVE® SPECIAL COMPOSITE ANCHOR

INSTALLATION STEPS FOR ROCK SLOPE STABILIZATION

- **STEP 5:** Injection of cement mixture and complete cementation of the strands within the bar to restore the full protection of the strands

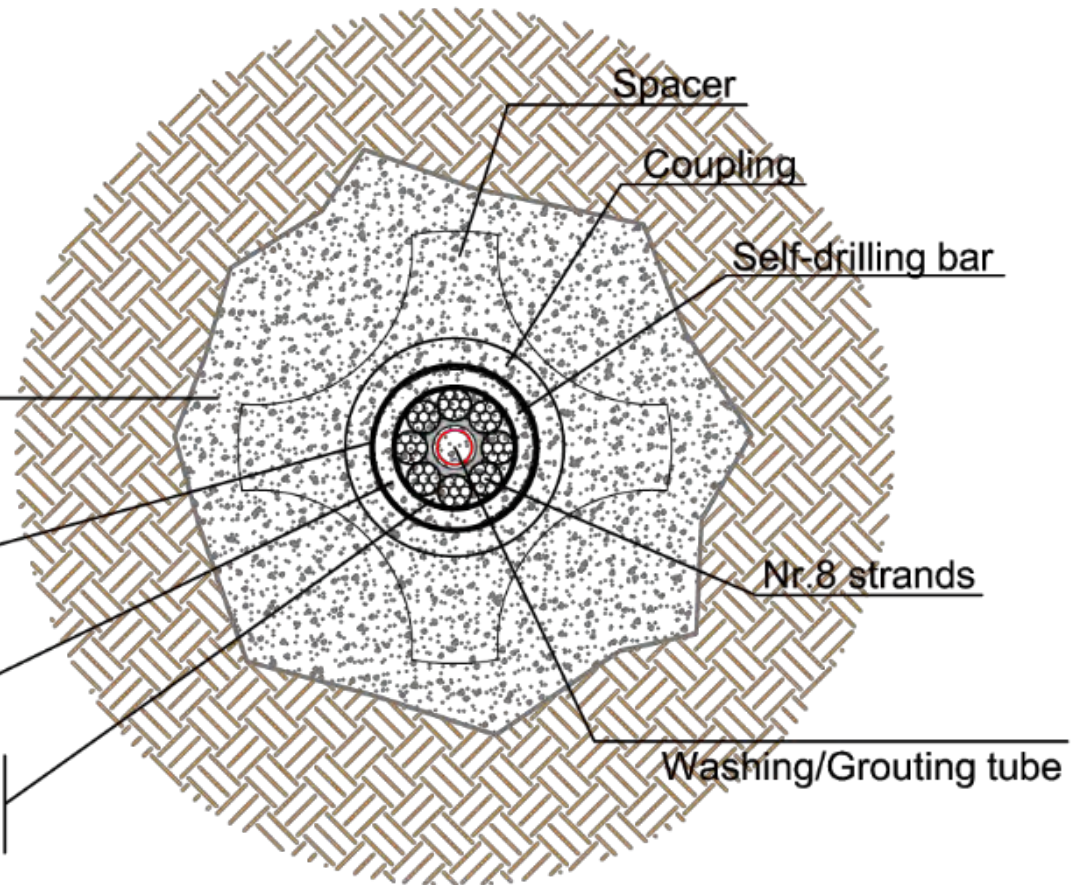


SIRIVE® SPECIAL COMPOSITE ANCHOR

PROTECTION

PROTECTION

- 1- Cement grout, dosage 40/100
- 2- Hot dip-galvanizing in accordance with UNI EN ISO 1461
- 3- Iron bar, thickness 8 mm, sacrificial anode
- 4- Internal injection, cement grout, dosage 40/100



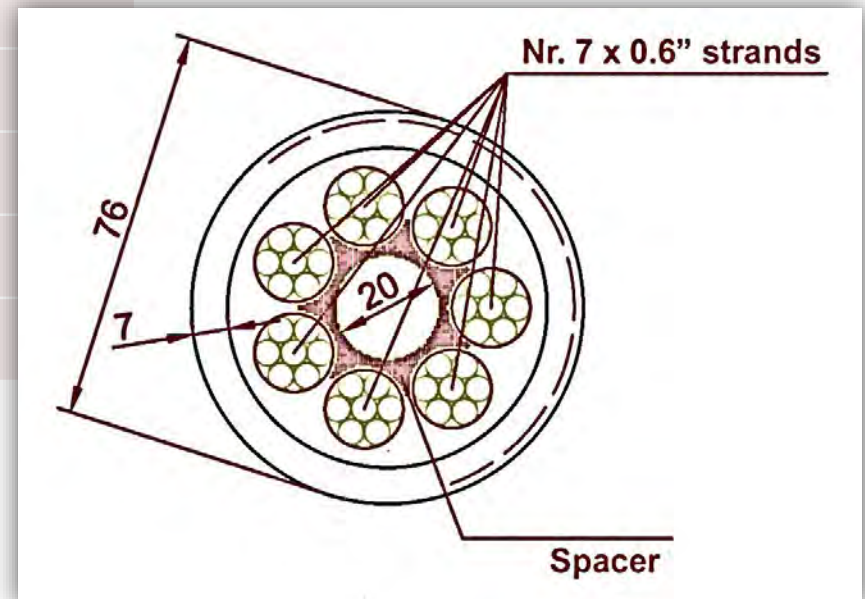
SIRIVE® SPECIAL COMPOSITE ANCHOR

ULTIMATE TENSILE LOADS

Anchor bar type	Ultimate tensile load (*) [kN]
R32 Special	550
R38 Special	700
R51 Special	1100
S60 Special	2000
S76 Special	3000
S90/A Special	4000
S90/B Special	5000

(*) Minimum warranted load

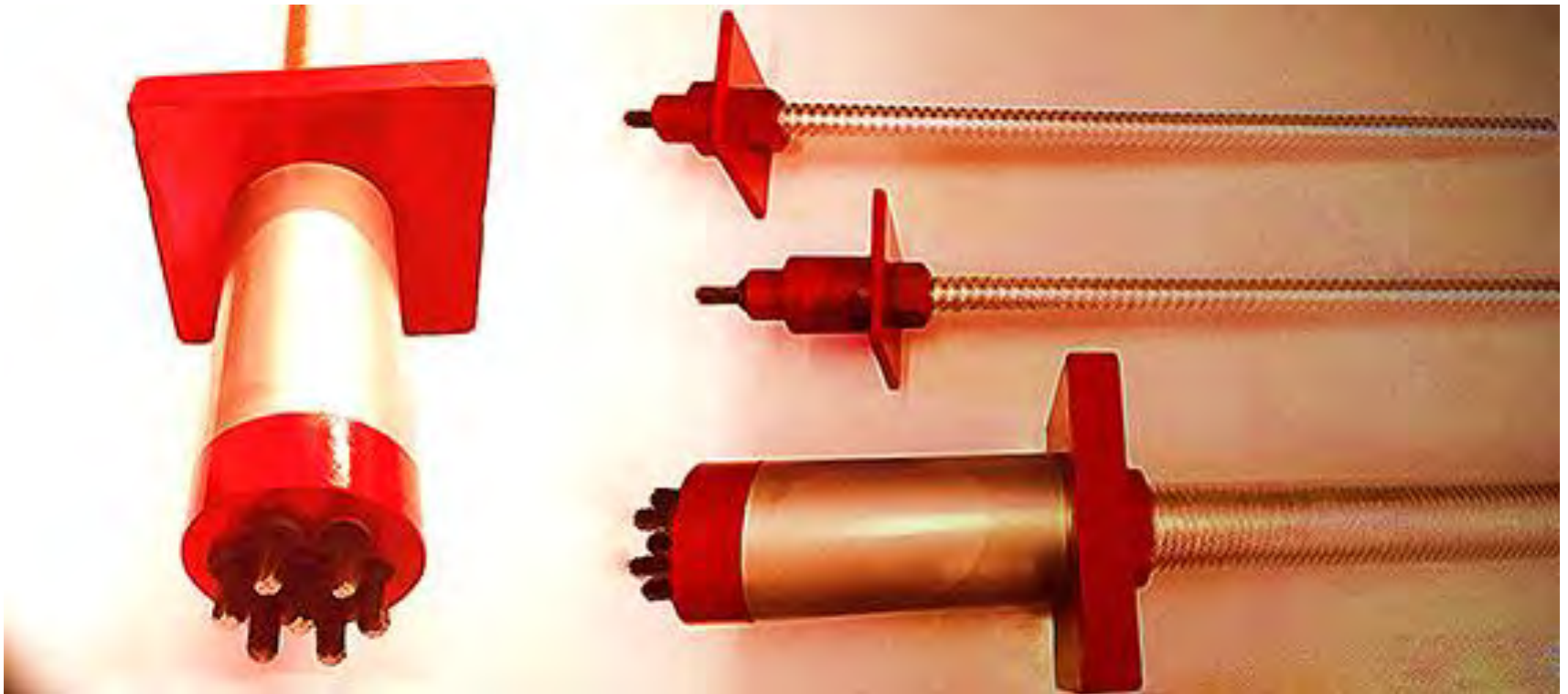
Sirive® Special Composite Anchor S76 CROSS SECTION



SIRIVE® SPECIAL COMPOSITE ANCHOR

ACCESSORIES

- **Sirive® Special Head Blocks**
(custom-made for both active and passive anchor configuration)



Sirive® Special Composite Anchor S76

SIRIVE® SPECIAL COMPOSITE ANCHOR

COST ANALYSIS

DESCRIPTION	COST [€/meter]		
	Self-drilling bar	Anchor with 12 Ø0,6"strands	Composite bar Ø76 8mm thick +8 Ø0,6"strands
Bar, Fe55, steel section 1800 mm ²			21.06
Nr. 8 strands, diameter 0.6"			8.00
Bar, Fe55, steel section 5455 mm ²	63.83		
Nr. 12 strands, diameter 0.6"		12.00	
Accessories and installation	67.00	69.00	42.85
Subtotal production costs	130.83	81.00	71.91
General costs: 8%	10.47	6.48	5.75
Subtotal	141.30	87.48	77.66
Profit for the enterprise: 30%	42.39	26.24	23.30
TOTAL COST	183.69	113.72	100.96
Saving with composite anchor %	45.0	11.2	-

Comparison of the cost of 3 alternative anchoring systems for a ultimate tensile strength of 3000 kN

SIRIVE® SPECIAL COMPOSITE ANCHOR

ADVANTAGES

- **Minor cost** at constant mechanical properties;
- High ultimate tensile strength and low elongation (serviceability);
- **Durability** (minor cracking, better protection from corrosion);
- Easy transport and quick **installation**;
- **Anchorage length is adaptable** to different geological and geotechnical conditions found *in situ*;
- **Increased flexural inertia and continuity** given by strand to the full reinforcement (improved if compared to simple coupling sleeve).



SIRIVE® FLOATING ANCHOR



SIRIVE® FLOATING ANCHOR

SEARCH FOR NEW SOLUTIONS

- **Lack of economic resources available** to meet the emergency.
- Search for new types of intervention:
 - ▣ Low cost;
 - ▣ Quick installation;
 - ▣ Environmental care.
- **«Floating Anchor» project**: partnership between University of Padova, Province of Vicenza and Dalla Gassa s.r.l.
- Stabilization of slopes subject to landslides with low to medium depth (up to 25 m deep).
- **SUMMARY:**
 - ▣ Technical/economical comparison between most commonly used strengthening intervention works;
 - ▣ The «floating anchor» technique;
 - ▣ Advantages.

SIRIVE® FLOATING ANCHOR

THE BASIC IDEA

□ What type of landslides? **Slow/Very slow**

Velocity Class	Description	Velocity (mm/sec)	Typical Velocity	Probable Destructive Significance
7	Extremely Rapid	5×10^3	5 m/sec	Catastrophe of major violence; buildings destroyed by impact of displaced material; many deaths; escape unlikely
6	Very Rapid	5×10^1	3 m/min	Some lives lost; velocity too great to permit all persons to escape
5	Rapid	5×10^{-1}	1.8 m/hr	Escape evacuation possible; structures; possessions, and equipment destroyed
4	Moderate	5×10^{-3}	13 m/month	Some temporary and insensitive structures can be temporarily maintained
3	Slow	5×10^{-5}	1.6 m/year	Remedial construction can be undertaken during movement; insensitive structures can be maintained with frequent maintenance work if total movement is not large during a particular acceleration phase
2	Very Slow	5×10^{-7}	15 mm/year	Some permanent structures undamaged by movement
	Extremely SLOW			Imperceptible without instruments; construction POSSIBLE WITH PRECAUTIONS

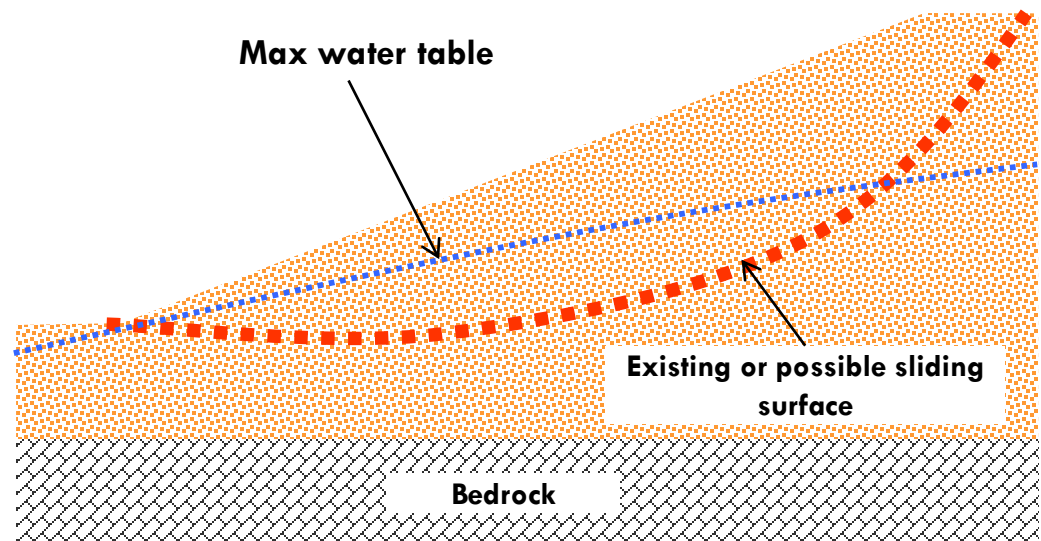
Cruden & Varnes
(1996)

SIRIVE® FLOATING ANCHOR

THE BASIC IDEA

- Slope stabilization with reinforcement provides for **increasing shear strength** or **reducing the sliding actions** along the slip surface with various types of structures:

- ▣ Retaining walls
- ▣ Dowels
- ▣ Micropiles
- ▣ Anchors
- ▣ Soil nailing

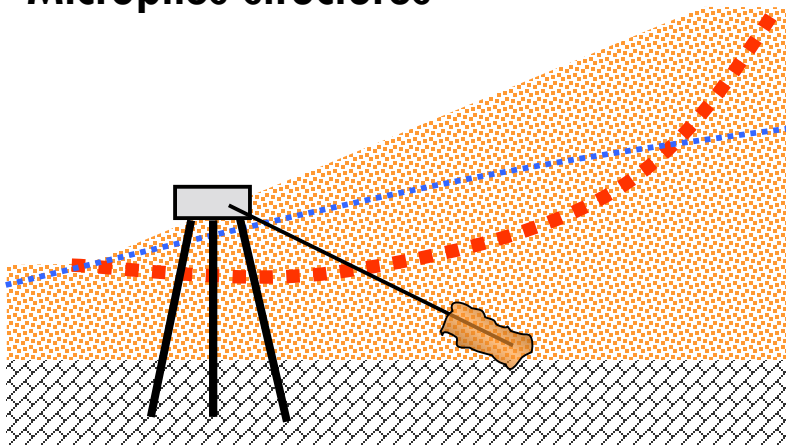


SIRIVE® FLOATING ANCHOR

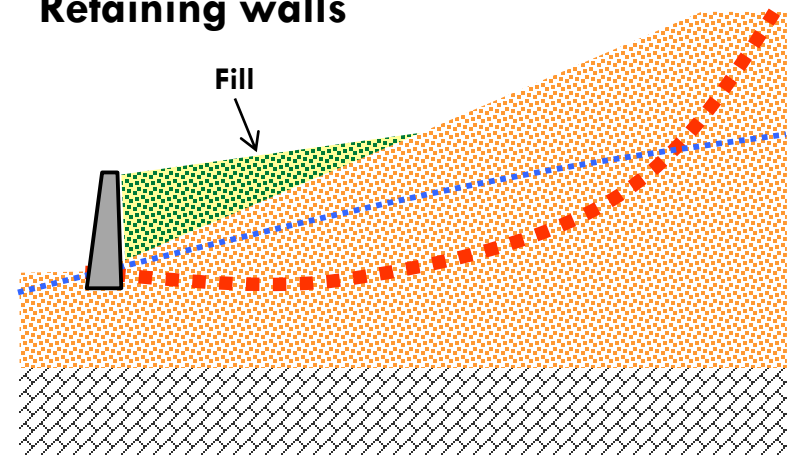
THE BASIC IDEA

- **Alternative to rigid techniques** normally used, which have some disadvantages:
 - ▣ Need for an accurate assessment of the acting forces (collapse);
 - ▣ High stiffness, poor adaptability to any movement of the slope;
 - ▣ High internal stresses;
 - ▣ Lack of modularity;
 - ▣ High costs ...

Micropiles structures



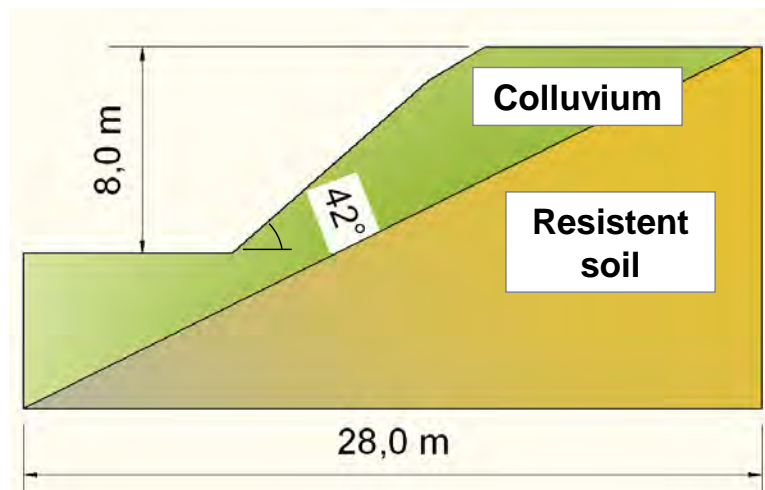
Retaining walls



TRADITIONAL REMEDIATION WORKS

A COST-EFFECTIVENESS COMPARISON

- Stabilization of a generic slope with a limited height.
- **Design** of the intervention according to Italian NTC 2008.
- **Limit equilibrium (LE) analysis.**
- Assessment of the **global safety factor** for the rotational instability.
- Assessment of the **intervention cost** per linear meter.



Formation	Type of soil	γ [kN/m ³]	c' [kPa]	ϕ [°]
Colluvium	Silty clayey sand	18	0	28
Bedrock	Gravel	19	0	38

TRADITIONAL REMEDIATION WORKS

A COST-EFFECTIVENESS COMPARISON

N.	Type of intervention	Characteristics of intervention	FS	Price ⁽¹⁾ (Euro/m)	Price/ Δ FS ⁽¹⁾ (Euro/m)
a	Cantilever wall	Height = 5,0 m; Width = 3,5 m; Depth of tooth = 0,7 m	1.29	1694	5841
b	Gabion wall	Height = 5,0 m; Width = 4,5 m; base dip = 6°	1.30	2614	8713
c	Reinforced earth wall	Height = 5,0 m; Width = 3,5 m	1.39	1360	3487
d	Dowels	Height = 2,0 m; Depth = 7,0 m; 1 lines of piles with 0,4 pile/m; D=60 cm; reinforcement rods 16Ø26	1.58	1781	3071
e	Wall founded on micropiles	Height = 2,8 m; Depth = 4,0 m; 2 micropile lines with spacing $i=0,2$; 0,66 micropile/m; $D_{ex}=114,3$ mm; $s=6,3$ mm; passive anchor R38 spacing 1,5 m; L = 10 m; $\alpha = 25^\circ$	1.60	1420	2367
f	Anchored micropile sheet-wall	Height = 2,5 m; Depth = 4,2 m; 2 micropile lines with spacing $i=0,5$; 2 micropile/m; $D_{ex}=127$ mm; $s=8$ mm; passive anchor R38 spacing 2,5 m; L = 12 m; $\alpha = 30^\circ$	1.46	1584	3443
g	Passive nails	L = 6, 6, 6, 9 m; $i_x = i_z = 1,6$ m; $\alpha = 15^\circ$; facing with steel net	1.39	883	2264

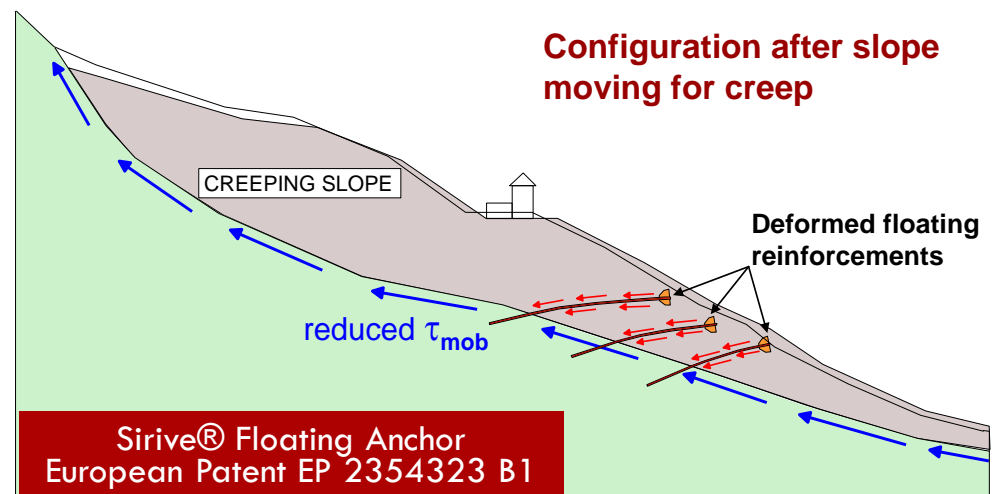
“Reinforcement works for the slope stabilization: standard and new approaches for the use of micropiles and anchors”

S. Cola, A. Bisson, C. Pilati, S. Frasson, G. Stevan, G. Tessari, ISM 2012: International Workshop on Micropiles, Milan, 2012

SIRIVE® FLOATING ANCHOR

A BRIEF INTRODUCTION

- Nails are designed to absorb significant horizontal stresses, thus **reducing the stresses that induce the viscous motion**, in order to slow down the evolution process of the landslides
- As opposed to active anchors, the floating anchor absorbs a part of the shear stresses induced by the landslide movement by mean of the **friction forces** activated along its profile
- In this way, it transfers to the external plate a small tension: it does not require a continuous facing, but only a small **head plate**



SIRIVE® FLOATING ANCHOR

A BRIEF INTRODUCTION

- External concrete plate (**floating element**) + nail (passive)
- The set is an “**energy dissipator**” that activates by **friction** within the moving slope (viscous medium)
- If the slope deforms and the ground moves, the plate may be engulfed into the soil



SIRIVE® FLOATING ANCHOR

A BRIEF INTRODUCTION

- Single reinforcing elements, each of them designed to absorb a fraction of the shear stress
- **Total ultimate pullout resistance** for one element:

$$Q_a = Q_p + \int_L \pi D \tau_u dx$$



Head force
(external plate)

Lateral friction
(passive bar)



SIRIVE® FLOATING ANCHOR

A BRIEF INTRODUCTION

- The system activation occurs with **relative displacements at the soil-concrete interface**. It may produce:
 - ▣ **Complete stabilization** of the slope: the axial force remains less than the maximum available axial strength;
 - ▣ **Only deceleration** of the slope: activation of the maximum available axial strength;
 - ▣ **In any case:** no structural failure of reinforcements.



SIRIVE® FLOATING ANCHOR

ADVANTAGES

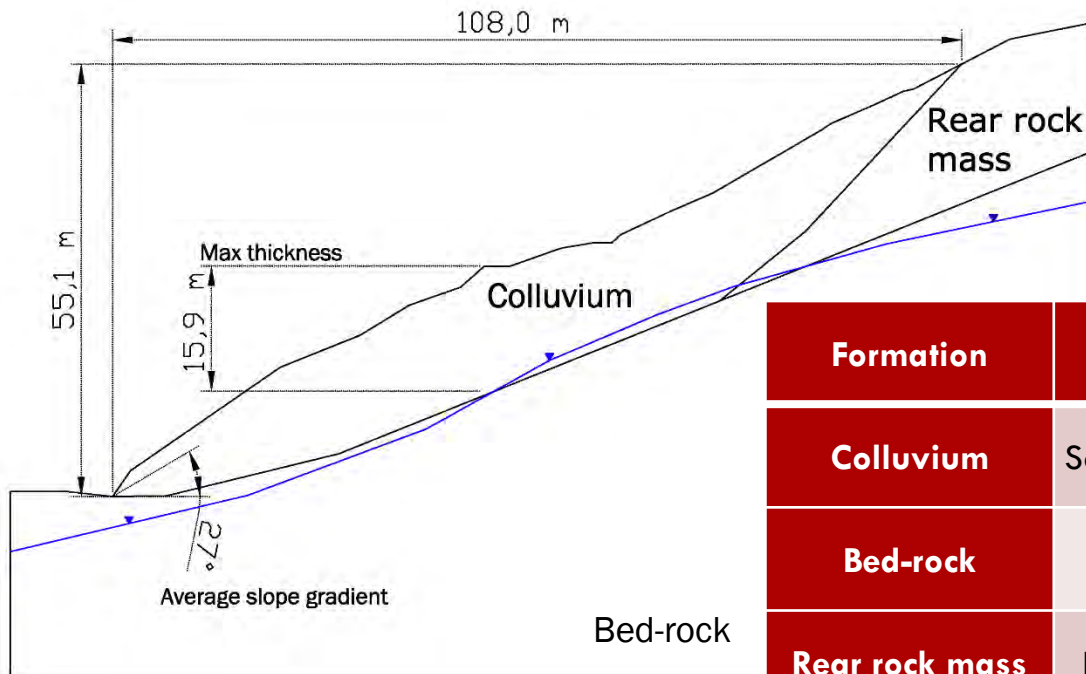
- Flexible, not rigid
- Modularity, **calibration** of the intervention work in progress
- Easy and quick to **install**
- Good protection against **corrosion** of the bars
- **Low environmental impact** (facing ratio about 5-6%)
- **Low cost**



GISBENTI LANDSLIDE

SIRIVE® SPECIAL COMPOSITE ANCHORS/SIRIVE® FLOATING ANCHORS

- Location Gisbenti, district of **Valli del Pasubio** (Vicenza, Italy).
- Stabilization work placed at the foot of a landslide (autumn 2010), **replacing a retaining wall** collapsed by slippage due to the landslide.
- 3 rows of floating anchors (Sirive® Special Composite Anchor S60, ultimate strength 2000 kN), 3 m horizontal spacing, 20 to 40 m long.



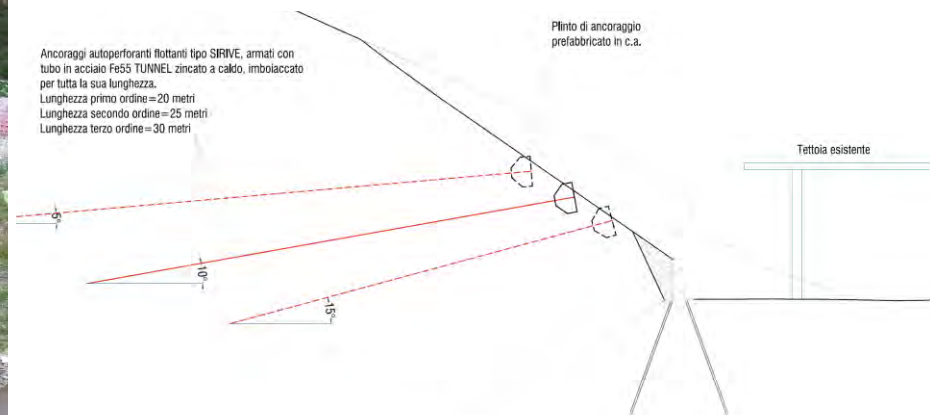
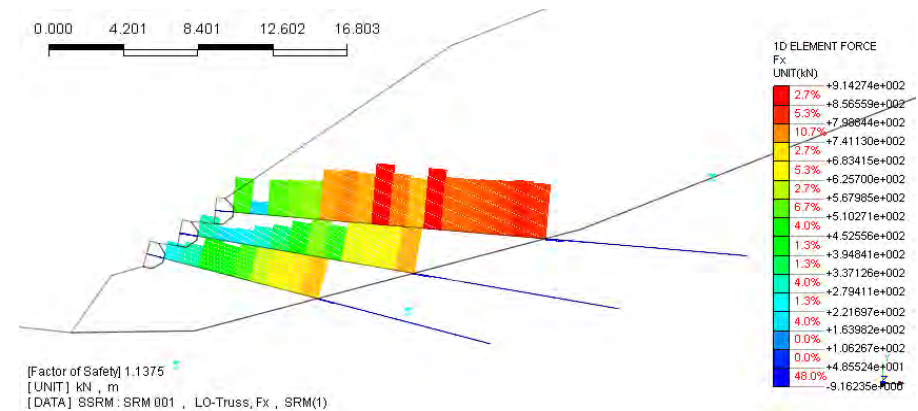
(Bisson A. & Cola S., 2014)

Formation	Soil	γ [kN/m ³]	c' [kPa]	ϕ [°]
Colluvium	Sandy clay	18	13	20
Bed-rock	Phyllites	24	150	35
Rear rock mass	Dolomite	22	300	36

GISBENTI LANDSLIDE

SIRIVE® SPECIAL COMPOSITE ANCHORS/SIRIVE® FLOATING ANCHORS

- **Maximum traction force** mobilized at the sliding surface to resist to destabilizing actions.
- **Low axial force behind the plates**, due to the balance of tangential shear stresses developed along the soil-grout interface along the bar.



VAL MASO LANDSLIDE

SIRIVE® SPECIAL COMPOSITE ANCHORS/SIRIVE® FLOATING ANCHORS

- Location Val Maso, district of Valli del Pasubio (Vicenza, Italy).
- Landslide reactivated in 2010 due to an **extreme rainfall**
- **Roto-translational collapse of about 200,000 m³** that threatened the stability of a road and produced a **small earth-flow** that damaged some houses
- Eluvial/colluvial deposits and past landslide debris
- Slope **mean inclination angle of about 40°**
- Landslide retrogression by multiple rotational slides, with a **sliding surface 20 m deep**



VAL MASO LANDSLIDE

SIRIVE® SPECIAL COMPOSITE ANCHORS/SIRIVE® FLOATING ANCHORS

- Adopting **Sirive® Special S60 Composite** anchor bars (60 mm diameter bars with 3x0.6" diameter strands and a minimum tensile strength of 2000 kN) anchored to the bedrock, **3 rows of floating anchors spaced 6.0 m and 6.0 m respectively in horizontal and vertical direction** were built.



VAL MASO LANDSLIDE

SIRIVE® SPECIAL COMPOSITE ANCHORS/SIRIVE® FLOATING ANCHORS

- Adopting **Sirive® Special S60 Composite** anchor bars (60 mm diameter bars with 3x0.6" diameter strands and a minimum tensile strength of 2000 kN) anchored to the bedrock, **3 rows of floating anchors spaced 6.0 m and 6.0 m respectively in horizontal and vertical direction** were built.



VAL MASO LANDSLIDE

MONITORING SYSTEM: DISPLACEMENTS



Leica TCRA1101
Total Station

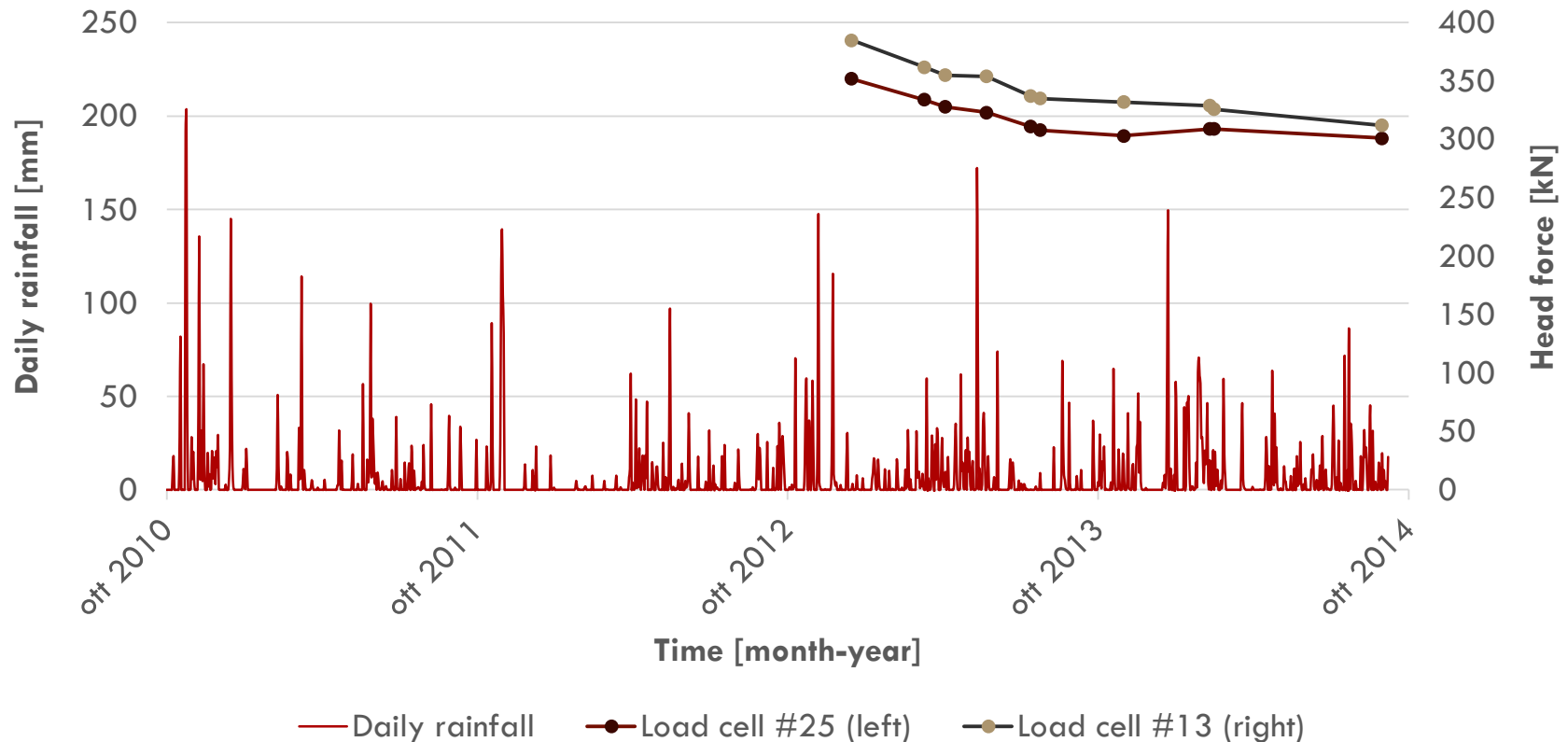
**Precision in
distance
measurements
= ± 2 mm**

Topographical survey:

- Determine displacements of 10 points selected on the slope and 30 on the plate of each anchor
- Landslide medium displ. rate = **2.6 cm/year (post) vs 160 cm/year (pre)**
Anchor medium displ. rate = 1.6 cm/year

VAL MASO LANDSLIDE

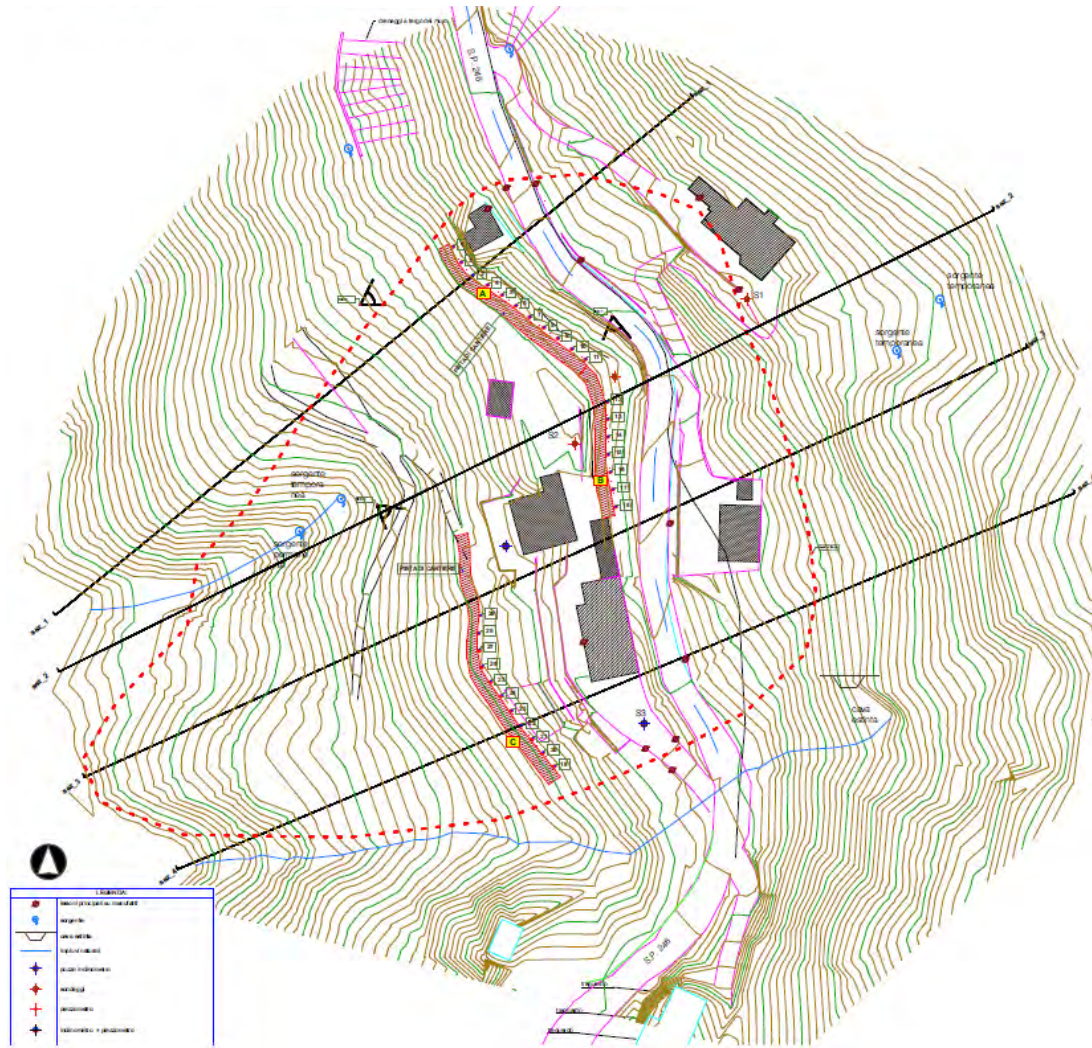
MONITORING SYSTEM: HEAD FORCE



The load cells indicate a small decrease of the head-forces in time (14.5-18.9%), which may denote a sort of **asymptotic adjustment** of the soil close to the concrete plates.

CISCHELE LANDSLIDE

SIRIVE® SPECIAL COMPOSITE ANCHORS/SIRIVE® FLOATING ANCHORS



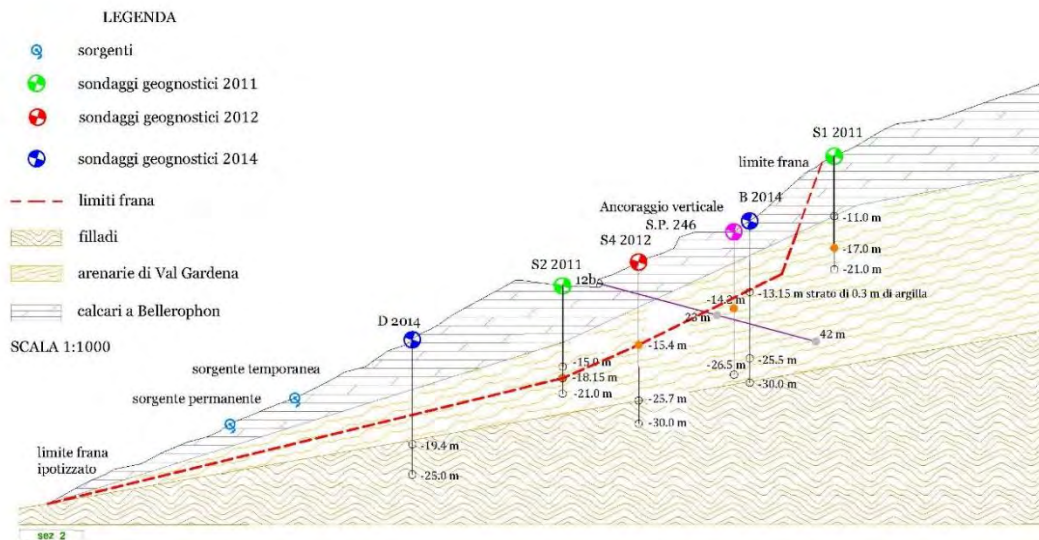
- Cross and longitudinal extent: 120 and 180 m
- Medium slope gradient: 24°
- Houses cracked and damaged



CISCHELE LANDSLIDE

SIRIVE® SPECIAL COMPOSITE ANCHORS/SIRIVE® FLOATING ANCHORS

- ❑ Slow-moving translational landslide
- ❑ Displacements are strongly correlated with the change in pore pressure
- ❑ 2 inclinometers: slip surface 18-20 m deep
- ❑ 33 floating anchors (Sirive® Special S76 Composite Anchors), 40 to 50 m long, 3000 kN ultimate tensile strength, 5 m horizontal spacing, frusto-conical concrete plates (1.5 m diameter)



CISCHELE LANDSLIDE

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THANK YOU

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www.sirive.it
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